## **Reliable Integer Ambiguity Resolution with Multi-Frequency Code Carrier Linear Combinations**

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### BIOGRAPHIES

Patrick Henkel studied electrical engineering and information technology at the Technische Universität München, Munich, Germany, and the École Polytechnique de Montréal, Canada. He then started his PhD on reliable carrier phase positioning and recently graduated with "summa cum laude". He is now working towards his habilitation in the field of precise point positioning. In 2007, he was a guest researcher at TU Delft, in 2008 at the GPS Lab at Stanford University, Stanford, CA. Patrick received the Pierre Contensou Gold Medal at the International Astronautical Congress in 2007, and the Bavarian regional prize at the European Satellite Navigation Competition together with Patryk Jurkowski in 2010.

Christoph Günther studied theoretical physics at the Swiss Federal Institute of Technology in Zurich. He received his diploma in 1979 and completed his PhD in 1984. He worked on communication and information theory at Brown Boveri and Ascom Tech. From 1995, he led the development of mobile phones for GSM and later dual mode GSM/Satellite phones at Ascom. In 1999, he became head of the research department of Ericsson in Nuremberg. Since 2003, he is the director of the Institute of Communication and Navigation at the German Aerospace Center (DLR) and since December 2004, he additionally holds a Chair at the Technische Universität München (TUM). His research interests are in satellite navigation, communication and signal processing.

### ABSTRACT

Carrier phase measurements are extremely accurate but ambiguous. The estimation of the integer ambiguities is in general split in two parts: A least-squares float solution, which is obtained by disregarding the integer property, and the actual fixing. The latter one can be a simple rounding, a sequential fixing (bootstrapping), or an integer least-squares estimation, which typically includes an integer decorrelation and a search. All these fixing methods suffer from a poor accuracy of the float solution due to the small carrier wavelengths. Moreover, the optimal integer least-squares estimation techniques are extremely sensitive to unknown biases.

This paper provides a new group of multi-frequency linear combinations to overcome the previous shortcomings: The combinations include both code and carrier phase measurements, and allow an arbitrary scaling of the geometry, an arbitrary scaling of the ionospheric delay, and any preferred wavelength. The maximization of the ambiguity discrimination results in combinations with a wavelength of several meters and a noise level of a few centimeters. These combinations are recommended for any application where reliability is more important than accuracy. Moreover, the paper provides an efficient method for the computation of the success rate of rounding.

### INTRODUCTION

Real-time kinematic (RTK) positioning uses double difference carrier phase measurements. The double differencing eliminates both receiver and satellite biases and clock offsets, which simplifies the resolution of the carrier phase integer ambiguities. Currently, there exist mainly three error sources that limit the reliability of the integer resolution: First, there is the double difference ionospheric delay, which only cancels for short baselines. Secondly, the double difference tropospheric delay is often neglected, which introduces some errors especially if there is a significant difference in the height between both receivers. The third and probably most challenging error source is multipath.

Fig. 1 shows the probability of wrong fixing for widelane ambiguity resolution as a function of the baseline length. We can observe a substantial increase in the failure rate if there is an ionospheric gradient of 1 mm/km between both receivers. It causes a double difference ionospheric delay which occurs as a bias in the ambiguity resolution. The probability of wrong fixings are shown in Fig. 1 for bootstrapping with and without integer decorrelation, whereas the latter one enables a certain improvement over the first one. Galileo double difference measurements on E1 and E5 were combined into an ionosphere-free code only combination and a phase-only combination with a wavelength of 78.2 cm. The latter combination amplifies the ionospheric delay by a factor 1.32. The failure rates significantly increase if the ionospheric gradient rises to 5 mm/km, which is still two orders of magnitude below the largest ionospheric gradient that has been observed so far. This is the motivation for the derivation and analysis of a new set of linear combinations, that enable an arbitrary scaling of the ionospheric delay and any preferred wavelength.



**Fig. 1** Reliability of widelane ambiguity resolution with double difference measurements.

# MULTI-FREQUENCY CODE CARRIER LINEAR COMBINATIONS

Multi-frequency linear combinations are an efficient approach to improve the reliability of carrier phase integer ambiguity resolution. The linear combinations enable a significant suppression of the ionospheric delay and an increase in the wavelength, while the range information is kept. A systematic search of all possible dual frequency phase-only widelane combinations has been performed by Cocard and Geiger in [1] and by Collins in [2]. An L1-L2 linear combination with a wavelength of 14.65 m was found. However, the combination also amplifies the ionospheric delay by more than 25 dB. The generalization to measurements on three and more frequencies enables much more attractive linear combinations as shown by Henkel and Günther in [3], by Wübbena in [4], or by Richert and El-Sheimy in [5]. For example, a Galileo triple frequency E1-E5a-E5b linear combination with a wavelength of 3.285 m suppresses the ionospheric delay by 17 dB. However, a complete elimination of the ionosphere is not achie-

vable with phase-only widelane combinations. Therefore, the authors suggested the inclusion of code measurements in the linear combination in [6]. The ambiguity discrimination was introduced as an optimization criterion for the combinations: It was defined as the ratio between the wavelength and twice the standard deviation of noise, which shall be maximized. The code measurements relax the integer constraint and enable the computation of a dual frequency geometry-preserving, ionosphere-free linear combination with a wavelength of 3.285 m and a noise level of a few centimeters. In [7], Henkel, Gomez and Günther presented multi-frequency code carrier linear combinations including the Galileo signals on E1, E5 and E6. In [8], Henkel gave a detailed derivation of code carrier combinations of maximum discrimination for an arbitrary number of frequencies.

In this section, the class of linear code carrier combinations is further generalized such that an arbitrary scaling of the geometry, an arbitrary scaling of the ionospheric delay, and any preferred wavelength are feasible. The code measurements from satellite k observed at user u on frequency m are modeled as

$$\rho_{u,m}^{k} = \|\boldsymbol{x}_{u} - \boldsymbol{x}^{k}\| + (\boldsymbol{e}_{u}^{k})^{T} \delta \boldsymbol{x}^{k} + c(\delta \tau_{u} - \delta \tau^{k}) 
+ T_{u}^{k} + q_{1m}^{2} I_{u,1}^{\prime k} + q_{1m}^{3} I_{u,1}^{\prime \prime k} + b_{\rho_{u,m}} + b_{\rho_{m}^{k}} 
+ \ddot{o}_{\rho_{u,m}^{k}} + \epsilon_{\rho_{u,m}^{k}},$$
(1)

with the user position  $x_u$ , the satellite position  $x^k$ , the unit vector  $e_u^k$  pointing from the satellite to the receiver, the satellite position error  $\delta x^k$  due to imperfect knowledge of the orbit, the receiver clock offset  $\delta \tau_u$ , the satellite clock offset  $\delta \tau^k$ , the speed of light c, the tropospheric delay  $T_u^k$ , the ratio of frequencies  $q_{1m} = f_1/f_m$ , the first and second order ionospheric delays  $\{I_{u,1}^{\prime k}, I_{u,1}^{\prime \prime k}\}$  on L1/E1, the receiver code bias  $b_{\rho_{u,m}}$ , the satellite code bias  $b_{\rho_m^k}$ , the delay  $\ddot{o}_{\rho_{u,m}^k}$ due to code multipath, and the code noise  $\epsilon_{\rho_{u,m}^k}$ . A similar model is used for the carrier phase measurements:

$$\lambda_{m}\phi_{u,m}^{k} = \|\boldsymbol{x}_{u} - \boldsymbol{x}^{k}\| + (\boldsymbol{e}_{u}^{k})^{T}\delta\boldsymbol{x}^{k} + c(\delta\tau_{u} - \delta\tau^{k}) + T_{u}^{k} - q_{1m}^{2}I_{u}^{\prime k} - \frac{1}{2}q_{1m}^{3}I_{u}^{\prime \prime k} + b_{\phi_{u,m}} + b_{\phi_{m}^{k}} + \ddot{o}_{\phi_{u,m}^{k}} + \lambda_{m}N_{u,m}^{k} + \varepsilon_{\phi_{u,m}^{k}}, \qquad (2)$$

with the wavelength  $\lambda_m$  and the carrier phase integer ambiguity  $N_{u,m}^k$ . The code and carrier phase measurements of (1) and (2) are linearly combined in (4) with the phase weight  $\alpha_m$  and the code weight  $\beta_m$ . The choice of these weights is obtained from some constraints on the geometry, ionospheric delay, combined multipath and biases, and a further optimization that shall be described later in this section. The first term on the right side of (4) describes the geometry term which can be scaled to any arbitrary value  $h_1$ , i.e.

$$\sum_{m=1}^{M} (\alpha_m + \beta_m) = h_1.$$
(3)

$$\sum_{m=1}^{M} (\alpha_{m} \lambda_{m} \phi_{u,m}^{k} + \beta_{m} \rho_{u,m}^{k}) = \left( \sum_{m=1}^{M} (\alpha_{m} + \beta_{m}) \right) \cdot \left( \| \boldsymbol{x}_{u} - \boldsymbol{x}^{k} \| + (\boldsymbol{e}_{u}^{k})^{T} \delta \boldsymbol{x}^{k} + c(\delta \tau_{u} - \delta \tau^{k}) + T_{u}^{k} \right) \\ + \left( \sum_{m=1}^{M} (\alpha_{m} - \beta_{m}) q_{1m}^{2} \right) \cdot I_{u,1}^{\prime k} + \left( \sum_{m=1}^{M} (\frac{1}{2} \alpha_{m} - \beta_{m}) q_{1m}^{3} \right) \cdot I_{u,1}^{\prime \prime k} \\ + \left( \sum_{m=1}^{M} \alpha_{m} \lambda_{m} N_{u,m}^{k} \right) + \left( \sum_{m=1}^{M} \alpha_{m} (b_{\phi_{u,m}} + b_{\phi_{m}^{k}}) + \beta_{m} (b_{\rho_{u,m}} + b_{\rho_{m}^{k}}) \right) \\ + \left( \sum_{m=1}^{M} (\alpha_{m} \ddot{o}_{\phi_{u,m}^{k}} + \beta_{m} \ddot{o}_{\rho_{u,m}^{k}}) \right) + \left( \sum_{m=1}^{M} (\alpha_{m} \varepsilon_{\phi_{u,m}^{k}} + \beta_{m} \varepsilon_{\rho_{u,m}^{k}}) \right)$$
(4)

A geometry-free combination is obtained if  $h_1 = 0$  and a geometry-preserving one if  $h_1 = 1$ . Note that the scaling of the geometry also affects the orbital error, the clock offsets and the tropospheric delay. The first order ionospheric delay  $I_{u,1}^{\prime k}$  can also be scaled by any arbitrary value  $h_2$ , i.e.

$$\sum_{m=1}^{M} (\alpha_m - \beta_m) q_{1m}^2 = h_2, \tag{5}$$

where  $h_2 = 0$  corresponds to an ionosphere-free and  $h_2 = -1$  to an ionosphere-preserving combination. However, a scaling factor in between -1 and 0 could be interesting if a certain ionospheric suppression is already achieved by double differencing. Similarly, the second order ionospheric delay can also be scaled by any value  $h_3$ , i.e.

$$\sum_{m=1}^{M} (\frac{1}{2}\alpha_m - \beta_m) q_{1m}^3 = h_3.$$
 (6)

The next term on the right side of (4) describes the linear combination of integer ambiguities which shall be a common wavelength  $\lambda$  times a single integer ambiguity  $N_u^k$ , i.e.

$$\sum_{m=1}^{M} \alpha_m \lambda_m N_{u,m}^k = \lambda N_u^k, \tag{7}$$

which can be easily solved for  $N_u^k$ :

$$N_{u}^{k} = \sum_{m=1}^{M} \underbrace{\frac{\alpha_{m} \lambda_{m}}{\lambda_{m}}}_{=j_{m}} N_{u,m}^{k}.$$
(8)

As  $N_{u,m}^k$  is an unknown integer,  $j_m$  has to be integer to obtain an integer  $N_u^k$ . Rearranging (8) gives the phase weight

$$\alpha_m = \frac{j_m \lambda}{\lambda_m},\tag{9}$$

which depends on the integer weight  $j_m$  and the combined wavelength  $\lambda$ . The next term on the right side of (4) includes the linear combination of code and carrier phase biases. It can also be considered in the combination design, e.g. by a pre-defined upper bound  $b_{\max}$  on the worst-case combined bias, i.e.

$$\sum_{m=1}^{M} |\alpha_m| (|b_{\phi_{u,m}}| + |b_{\phi_m^k}|) + |\beta_m| (|b_{\rho_{u,m}}| + |b_{\rho_m^k}|) \le b_{\max},$$
(10)

which requires some assumptions on the measurement biases. The superposition of multipath delays can also be included in the combination design, e.g. by

$$\sum_{m=1}^{M} |\alpha_m| \cdot |\ddot{o}_{\phi_{u,m}^k}| + |\beta_m| \cdot |\ddot{o}_{\rho_{u,m}^k}| \le \ddot{o}_{\max}, \qquad (11)$$

with some pre-defined upper bound  $\ddot{o}_{\max}$  on the worst-case superposition of multipath-delays. These could be chosen from an elevation-dependant exponential function, i.e.

$$\ddot{o}_{\phi_{u,m}^{k}} = \ddot{o}_{0} \cdot e^{-\frac{E}{\gamma}},\tag{12}$$

with the decay constant  $\gamma$  and elevation angle *E*. Finally, the last term on the right side of (4) describes the linear combination of phase and code noises. Its variance is given by

$$\sigma^2 = \sum_{m=1}^{M} \left( \alpha_m^2 \sigma_{\varepsilon_{\phi_{u,m}^k}}^2 + \beta_m^2 \sigma_{\varepsilon_{\rho_{u,m}^k}}^2 \right), \qquad (13)$$

and can be minimized under the consideration of all other constraints. Alternatively, the ambiguity discrimination can be maximized. It was first introduced by Henkel and Günther in [6] as

$$D = \frac{\lambda}{2\sigma}.$$
 (14)

Its maximization corresponds to the minimization of the probability of wrong fixing for a geometry-free, ionosphere-free linear combination. As this paper is focussing more on the reliability than on the accuracy, the further analysis is restricted to the class of linear combinations that maximize D. Let us start the derivation of the optimum  $\alpha_m$  and  $\beta_m$  by introducing the total phase weight

$$w_{\phi} = \sum_{m=1}^{M} \alpha_m = \lambda \sum_{m=1}^{M} \frac{j_m}{\lambda_m},$$
(15)

which can be solved for the combined wavelength  $\lambda$ , i.e.

$$\lambda = \frac{w_{\phi}}{\sum\limits_{m=1}^{M} \frac{j_m}{\lambda_m}}.$$
(16)

Replacing  $\lambda$  in (9) by (16) gives

$$\alpha_m = \frac{j_m}{\lambda_m} \lambda = \frac{j_m}{\lambda_m} \frac{1}{\sum\limits_{m=1}^M \frac{j_m}{\lambda_m}} w_\phi.$$
(17)

The constraints on the geometry and first order ionospheric delay are written in matrix-vector notation using (3), (5) and (17), i.e.

$$\Psi_1 \begin{bmatrix} \beta_1 \\ \beta_2 \end{bmatrix} + \Psi_2 \begin{bmatrix} w_{\phi} \\ \beta_3 \\ \vdots \\ \beta_M \end{bmatrix} = \begin{bmatrix} h_1 \\ h_2 \end{bmatrix}, \quad (18)$$

with

$$\Psi_1 = \begin{bmatrix} 1 & 1\\ -1 & -q_{12}^2 \end{bmatrix} \tag{19}$$

and

$$\Psi_{2} = \begin{bmatrix} 1 & 1 & \dots & 1\\ \sum_{m=1}^{M} \frac{j_{m}}{\lambda_{m}} \frac{1}{\sum_{m=1}^{M} \frac{j_{m}}{\lambda_{m}}} q_{1m}^{2} & -q_{13}^{2} & \dots & q_{1M}^{2} \end{bmatrix}.$$
(20)

Note that the second order ionospheric delay has not been included in (18) as it is often negligible. Eq. (18) can be solved for the code weights  $\beta_1$  and  $\beta_2$ :

$$\begin{bmatrix} \beta_{1} \\ \beta_{2} \end{bmatrix} = \Psi_{1}^{-1} \left( \begin{bmatrix} h_{1} \\ h_{2} \end{bmatrix} - \Psi_{2} \begin{bmatrix} w_{\phi} \\ \beta_{3} \\ \vdots \\ \beta_{M} \end{bmatrix} \right)$$
$$= \begin{bmatrix} s_{1} + s_{2}w_{\phi} + \sum_{m=3}^{M} s_{m}\beta_{m} \\ t_{1} + t_{2}w_{\phi} + \sum_{m=3}^{M} t_{m}\beta_{m} \end{bmatrix}, \quad (21)$$

where the  $s_m$  and  $t_m$ ,  $m \in \{1, \ldots, M\}$  are implicitly defined by the last equality. Equation (21) leaves the integer coefficients  $j_m$ ,  $m \ge 1$ , the code weights  $\beta_m$ ,  $m \ge 3$ , and the total phase weight  $w_{\phi}$  as unknowns. The maximization of D over these variables shall be performed in two steps as shown in Fig. 2.



**Fig. 2** Computation of multi-frequency code carrier linear combinations of maximum ambiguity discrimination

First, a numerical search is performed with a maximization over  $j_m$  and, secondly, an analytical computation is performed with a maximization over  $w_{\phi}$  and  $\beta_m$ . Equation (28) provides an expression of the ambiguity discrimination that is obtained from (14) using (16), (17), (21) and (13), and only depends on  $w_{\phi}$  and  $\beta$ . Some abbreviations were introduced to simplify the notation:

$$\tilde{\eta}^2 = \sum_{m=1}^M \frac{j_m^2}{\lambda_m^2} \frac{1}{\left(\sum_{m=1}^M \frac{j_m}{\lambda_m}\right)^2} \sigma_{\phi_m}^2, \qquad (22)$$

$$\Sigma = \begin{bmatrix} \sigma_{\rho_3}^2 & \dots & \sigma_{\rho_3\rho_M} \\ \vdots & \ddots & \vdots \\ \sigma_{\rho_3\rho_M} & \dots & \sigma_{\rho_M}^2 \end{bmatrix}, \quad (23)$$

as well as  $\boldsymbol{\beta} = [\beta_3, \dots, \beta_M]^T$ ,  $\boldsymbol{s} = [s_3, \dots, s_M]^T$ , and  $\boldsymbol{t} = [t_3, \dots, t_M]^T$ . The maximization with respect to  $w_{\phi}$  results in the constraint

$$\frac{\partial D}{\partial w_{\phi}} \stackrel{!}{=} 0, \tag{24}$$

and the maximization with respect to  $\beta$  gives

$$\frac{\partial D}{\partial \boldsymbol{\beta}} \stackrel{!}{=} \boldsymbol{0}.$$
 (25)

The latter constraint can be developed as

$$(s_1 + s_2 w_{\phi} + \boldsymbol{s}^T \boldsymbol{\beta}) \boldsymbol{s} \cdot \boldsymbol{\sigma}_{\rho_1}^2$$

$$+ (t_1 + t_2 w_{\phi} + \boldsymbol{t}^T \boldsymbol{\beta}) \boldsymbol{t} \cdot \boldsymbol{\sigma}_{\rho_2}^2 + \boldsymbol{\Sigma} \boldsymbol{\beta}$$

$$= \boldsymbol{\sigma}_{\rho_1}^2 \boldsymbol{s}(s_1 + s_2 w_{\phi} + \boldsymbol{s}^T \boldsymbol{\beta}) + \boldsymbol{\sigma}_{\rho_2}^2 \boldsymbol{t}(t_1 + t_2 w_{\phi} + \boldsymbol{t}^T \boldsymbol{\beta})$$

$$+ \boldsymbol{\Sigma} \boldsymbol{\beta}$$

$$(26)$$

$$= \underbrace{\left[\sigma_{\rho_{1}}^{2} s s^{T} + \sigma_{\rho_{2}}^{2} t t^{T} + \Sigma\right]}_{A} \beta$$

$$+ \underbrace{\left[s_{2} \sigma_{\rho_{1}}^{2} s + t_{2} \sigma_{\rho_{2}}^{2} t\right]}_{b} w_{\phi} + \underbrace{\left[s_{1} \sigma_{\rho_{1}}^{2} s + t_{1} \sigma_{\rho_{2}}^{2} t\right]}_{c} = 0,$$
(27)

$$D(w_{\phi}, \beta) = \frac{\lambda}{2\sigma} = \frac{w_{\phi}}{\sum_{m=1}^{M} \frac{j_m}{\lambda_m}} \frac{1}{2\sqrt{\tilde{\eta}^2 w_{\phi}^2 + (s_1 + s_2 w_{\phi} + \boldsymbol{s}^T \beta)^2 \sigma_{\rho_1}^2 + (t_1 + t_2 w_{\phi} + \boldsymbol{t}^T \beta)^2 \sigma_{\rho_2}^2 + \beta^T \boldsymbol{\Sigma} \beta}$$
(28)

which shows a linear relationship between  $w_{\phi}$  and  $\beta$ . Solving (26) for  $\beta$  yields

$$\boldsymbol{\beta} = -\boldsymbol{A}^{-1}(\boldsymbol{c} + \boldsymbol{b} \cdot \boldsymbol{w}_{\phi}). \tag{29}$$

The first constraint in (24) can also be further developed as

$$(s_1 + s_2 w_{\phi} + \boldsymbol{s}^T \boldsymbol{\beta}) (s_1 + \boldsymbol{s}^T \boldsymbol{\beta}) \sigma_{\rho_1}^2 + (t_1 + t_2 w_{\phi} + \boldsymbol{t}^T \boldsymbol{\beta}) (t_1 + \boldsymbol{t}^T \boldsymbol{\beta}) \sigma_{\rho_2}^2 + \boldsymbol{\beta}^T \boldsymbol{\Sigma} \boldsymbol{\beta} = 0,$$

and replacing  $\beta$  by (29) gives

$$(s_1 + s_2 w_{\phi} - s^T A^{-1} (\boldsymbol{c} + \boldsymbol{b} w_{\phi}))$$
  

$$\cdot (s_1 - s^T A^{-1} (\boldsymbol{c} + \boldsymbol{b} w_{\phi})) \cdot \sigma_{\rho_1}^2$$
  

$$+ (t_1 + t_2 w_{\phi} - \boldsymbol{t}^T A^{-1} (\boldsymbol{c} + \boldsymbol{b} w_{\phi}))$$
  

$$\cdot (t_1 - \boldsymbol{t}^T A^{-1} (\boldsymbol{c} + \boldsymbol{b} w_{\phi})) \cdot \sigma_{\rho_2}^2$$
  

$$+ (\boldsymbol{c} + \boldsymbol{b} w_{\phi})^T (\boldsymbol{A}^{-1})^T \boldsymbol{\Sigma} \boldsymbol{A}^{-1} (\boldsymbol{c} + \boldsymbol{b} w_{\phi}) = 0, \quad (30)$$

which only includes  $w_{\phi}$  (and  $j_m$ , hidden in A, b, c, s and t) as unknowns. Equation (30) is a quadratic equation in  $w_{\phi}$ , i.e.

$$r_0 + r_1 \cdot w_\phi + r_2 \cdot w_\phi^2 = 0, \tag{31}$$

with

$$r_{0} = (s_{1} - s^{T} A^{-1} c)^{2} \sigma_{\rho_{1}}^{2} + (t_{1} - t^{T} A^{-1} c)^{2} \sigma_{\rho_{2}}^{2} + c^{T} (A^{-1})^{T} \Sigma A^{-1} c$$
  
$$r_{1} = ((s_{1} - s^{T} A^{-1} c) (-s^{T} A^{-1} b) + (s_{2} - s^{T} A^{-1} b) (s_{1} - s^{T} A^{-1} c)) \cdot \sigma_{\rho_{1}}^{2} + ((t_{1} - t^{T} A^{-1} c) (-t^{T} A^{-1} b) + (t_{2} - t^{T} A^{-1} b) (t_{1} - t^{T} A^{-1} c)) \cdot \sigma_{\rho_{2}}^{2} + (c^{T} (A^{-1})^{T} \Sigma A^{-1} b + b^{T} (A^{-1})^{T} \Sigma A^{-1} c) r_{2} = (s_{2} - s^{T} A^{-1} b) (-s^{T} A^{-1} b) \cdot \sigma_{\rho_{1}}^{2} + (t_{2} - t^{T} A^{-1} b) (-t^{T} A^{-1} b) \cdot \sigma_{\rho_{2}}^{2} + b^{T} (A^{-1})^{T} \Sigma A^{-1} b.$$
(32)

The latter term  $r_2$  always vanishes which can be proven by replacing A, b, c, s and t by their definitions. Thus, the optimal total phase weight is given by

$$w_{\phi_{\text{opt}}} = -\frac{r_0}{r_1}.$$
(33)

The optimal phase and code weights  $\alpha_m$  and  $\beta_m$  are then obtained from (29), (21), and (17). The  $\alpha_m$  and  $\beta_m$  can be optimized for any standard deviation  $\sigma_{\rho_m}$ . In this paper, the

 $\sigma_{\rho_m}$  are chosen according to the Cramer Rao bound, which is given by

$$\Gamma_m = \sqrt{\frac{c^2}{\frac{C}{N_0}T_i \cdot \frac{\int (2\pi f)^2 |S_m(f)|^2 df}{\int |S_m(f)|^2 df}},$$
(34)

with the speed of light c, the carrier to noise power ratio  $\frac{C}{N_0}$ , the pre-detection integration time  $T_i$ , and the power spectral density  $S_m(f)$ . The latter one has been derived by Betz in [9] for binary offset carrier (BOC) modulated signals. Tab. 1 shows the Cramer Rao bounds of the wideband Galileo signals, which are used in the further analysis.

**Tab. 1** Cramer Rao Bounds for  $C/N_0 = 45$ dB-Hz and  $T_i = 1$ s

	Signal	BW [MHz]	Γ [cm]
E1	MBOC	20	11.14
E5	AltBOC(15,10)	51	1.95
E5a	BPSK(10)	20	7.83
E5b	BPSK(10)	20	7.83
E6	BPSK(5)	20	11.36

Tab. 2, 3 and 4 show the optimized dual, triple and four frequency code carrier widelane combinations of maximum discrimination for  $\sigma_{\phi} = 1$ mm and  $\sigma_{\rho_m} = \Gamma_m$ . The first line in each table represents a geometry-preserving (GP) ionosphere-free (IF) combination, followed by a GP reduced ionosphere (IR, 10 dB suppression) combination that can be used for positioning. The next linear combination is a geometry-free (GF), ionosphere-preserving (IP) one, which could be applied for the estimation of the ionospheric delay. The last combination is both GF and IF, which makes it a candidate for ambiguity resolution, or multipath analysis. The linear combinations are characterized by a wavelength of a few meters and a noise level of several centimeters, which results in a large ambiguity discrimination D. The GP-IF combination tends to a slightly larger D than the GF-IP one but both discriminations are large enough to enable a reliable integer ambiguity resolution if multipath and biases can be estimated. A comparison of Tab. 2 and Tab. 3 shows that the processing of the E5 signal as a single wideband signal is preferred over the processing of two subbands, i.e. the lower code noise of the AltBOC signal more than compensates for the slightly reduced number of degrees of freedom. The inclusion of E6 measurements further increases the ambiguity discrimination, which achieves its highest value for the E5a-E5b widelane ambiguity combination. Note also that all code coefficients  $\beta_m$  of the triple and four frequency GF-IF combinations are quite

$h_1$	$h_2$		E1		E5	$\lambda$	σ	D
1	0	$j_1$	17.0000	$j_2$	-1	2.005	C F	25.12
		$\begin{array}{c} \alpha_1 \\ \beta_1 \end{array}$	-0.0552	$\begin{array}{c} \alpha_2 \\ \beta_2 \end{array}$	-13.0593 -3.1484	3.285 m	6.5 cm	25.12
1	-0.1	$j_1$	1	$j_2$	-1			
		$\alpha_1$	16.2508	$\alpha_2$	-12.2936	3.092  m	6.1 cm	25.55
		$\beta_1$	-0.0487	$\beta_2$	-2.9085			
0	-1	$j_1$	-1	$j_2$	1			
		$\alpha_1$	-10.1831	$\alpha_2$	7.7035	1.938 m	4.9 cm	19.65
		$\beta_1$	0.0737	$\beta_2$	2.4059			
0	0	$j_1$	-1	$j_2$	1			
		$\alpha_1$	-5.2550	$\alpha_2$	3.9754	1 m	8.2 cm	6.09
		$\beta_1$	0.7285	$\beta_2$	0.5511			
$h_1$	$h_2$	E1		E5a		$\lambda$ $\sigma$		D
1	0	$j_1$	1	$j_2$	-1			
		$\alpha_1$	22.6467	$\alpha_2$	-16.9115	4.309 m	31.4 cm	6.87
		$\beta_1$	-1.0227	$\beta_2$	-3.7125			

**Tab. 2** Dual-frequency code carrier widelane combinations of maximum discrimination for  $\sigma_{\phi} = 1$ mm and  $\sigma_{\rho_m} = \Gamma_m$ 

**Tab. 3** Triple-frequency code carrier widelane combinations of maximum discrimination for  $\sigma_{\phi} = 1$ mm and  $\sigma_{\rho_m} = \Gamma_m$ 

$h_1$	$h_2$		E1	E5b			E5a	λ	σ	D
1	0	$j_1$	1	$j_2$	-4	$j_3$	3			
		$\alpha_1$	18.9326	$\alpha_2$	-58.0271	$\alpha_3$	42.4139	$3.603 \mathrm{m}$	$13.9~{\rm cm}$	12.99
		$\beta_1$	-0.2871	$\beta_2$	-0.9899	$\beta_3$	-1.0423			
1	-0.1	$j_1$	1	$j_2$	-4	$j_3$	3			
		$\alpha_1$	17.6991	$\alpha_2$	-54.2465	$\alpha_3$	39.6505	3.368  m	$12.7~\mathrm{cm}$	13.26
		$\beta_1$	-0.2499	$\beta_2$	-0.9013	$\beta_3$	-0.9519			
0	-1	$j_1$	1	$j_2$	-4	$j_3$	3			
		$\alpha_1$	-12.8901	$\alpha_2$	39.5074	$\alpha_3$	-28.8772	$2.543~\mathrm{m}$	$12.3~{\rm cm}$	9.98
		$\beta_1$	0.4477	$\beta_2$	0.9061	$\beta_3$	0.9061			
0	0	$j_1$	0	$j_2$	-1	$j_3$	1			
		$\alpha_1$	0	$\alpha_2$	-4.0266	$\alpha_3$	3.9242	1 m	0.8 cm	62.71
		$\beta_1$	0.0004	$\beta_2$	0.0480	$\beta_3$	0.0540			

**Tab. 4** Four-frequency code carrier widelane combinations of maximum discrimination for  $\sigma_{\phi} = 1$ mm and  $\sigma_{\rho_m} = \Gamma_m$ 

$h_1$	$h_2$		E1		E6		E5b	E5a		λ	σ	D
1	0	$j_1$	1	$j_2$	-3	$j_3$	0	$j_4$	2			
		$\alpha_1$	21.0108	$\alpha_2$	-51.1627	$\alpha_3$	0	$\alpha_4$	31.3798	$3.998 \mathrm{m}$	$6.5~\mathrm{cm}$	31.02
		$\beta_1$	-0.0239	$\beta_2$	-0.0349	$\beta_3$	-0.0824	$\beta_4$	-0.0867			
1	-0.1	$j_1$	1	$j_2$	-3	$j_3$	0	$j_4$	2			
		$\alpha_1$	19.7197	$\alpha_2$	-48.0187	$\alpha_3$	0	$\alpha_4$	29.4514	$3.753 \mathrm{~m}$	$6.0 \mathrm{~cm}$	31.22
		$\beta_1$	-0.0154	$\beta_2$	-0.0233	$\beta_3$	-0.0554	$\beta_4$	-0.0585			
0	-1	$j_1$	-1	$j_2$	4	$j_3$	-1	$j_4$	-2			
		$\alpha_1$	-13.1658	$\alpha_2$	42.7460	$\alpha_3$	-10.0881	$\alpha_4$	-19.6632	$2.505~\mathrm{m}$	$5.1~{ m cm}$	24.81
		$\beta_1$	0.0285	$\beta_2$	0.0274	$\beta_3$	0.0576	$\beta_4$	0.0576			
0	0	$j_1$	0	$j_2$	0	$j_3$	-1	$j_4$	1			
		$\alpha_1$	0	$\alpha_2$	0	$\alpha_3$	-4.0266	$\alpha_4$	3.9242	1 m	$0.8\mathrm{cm}$	64.27
		$\beta_1$	-0.0038	$\beta_2$	0.0140	$\beta_3$	0.0429	$\beta_4$	0.0493			

small, which indicates a large robustness over code multipath.

The search of the optimal integer coefficients  $j_m$  was performed over  $|j_m| \leq 4$ , and further constrained by  $\sigma < 0.4$ m to prevent combinations of extremely large wavelengths, that result in a large noise level. The wavelength of the GF, IF linear combination was set to 1 m as these type of combinations leave one degree of freedom: The discrimination is independent of  $\lambda$  and both the GF and IF constraints are fulfilled for any  $\lambda$ .

### **RELIABLE INTEGER AMBIGUITY RESOLUTION**

In this section, the linear combinations of the previous section are used for reliable integer ambiguity resolution. The following model is used for the code and carrier phase measurements from all visible satellites:

$$\Psi = H\xi + AN + \eta, \tag{35}$$

where H denotes the geometry matrix,  $\boldsymbol{\xi}$  includes all unknown real-valued parameters, A is the wavelength matrix, N are the integer ambiguities and  $\eta \sim \mathcal{N}(0, \Sigma)$  is the white Gaussian measurement noise. Note that  $\Psi$  can either consist of uncombined code and carrier phase measurements (traditional approach), or of two optimized GP linear combinations (our approach): a code carrier combination of maximum discrimination and a code-only combination of minimum noise amplification. In both cases, the estimation of  $\boldsymbol{\xi}$  can be separated from the integer ambiguity resolution by an orthogonal projection, i.e.

$$\boldsymbol{P}_{H}^{\perp}\boldsymbol{\Psi} = \underbrace{\boldsymbol{P}_{H}^{\perp}\boldsymbol{A}}_{\bar{\boldsymbol{A}}}\boldsymbol{N} + \boldsymbol{P}_{H}^{\perp}\boldsymbol{\eta}, \qquad (36)$$

with  $P_H^{\perp} = 1 - H(H^T \Sigma^{-1} H)^{-1} H^T \Sigma^{-1}$ . The least-squares float ambiguity solution follows from (36) as

$$\hat{N} = \left(\bar{A}\Sigma^{-1}\bar{A}\right)^{-1}\bar{A}^{T}\Sigma^{-1}\Psi$$
(37)

with the covariance

$$\boldsymbol{\Sigma}_{\hat{N}} = \left(\bar{\boldsymbol{A}}\boldsymbol{\Sigma}^{-1}\bar{\boldsymbol{A}}\right)^{-1}.$$
(38)

The most simple integer estimation technique is rounding of the float solution of (37). The success rate heavily depends on the conditioning of the equation system. It is characterized by the condition number which is defined as the ratio between the largest and smallest eigenvalue of  $\Sigma_{\hat{N}}$ . The success rate can be increased by a sequential integer estimation which also takes the correlation between the float estimates into account. It was introduced by Blewitt in [11] and is given by

$$\hat{N}_{k|1,\dots,k-1} = \hat{N}_{k} - \sum_{j=1}^{k-1} \sigma_{\hat{N}_{k}\hat{N}_{j|1,\dots,j-1}} \sigma_{\hat{N}_{j|1,\dots,j-1}}^{-2} \\
\cdot (\hat{N}_{j|1,\dots,j-1} - [\hat{N}_{j|1,\dots,j-1}]), \quad (39)$$

with the conditional variance

$$\sigma_{\hat{N}_{k|1,\dots,k-1}}^{2} = \sigma_{\hat{N}_{k}}^{2} - \sum_{j=1}^{k-1} \sigma_{\hat{N}_{k}\hat{N}_{j|1,\dots,j-1}}^{2} \sigma_{\hat{N}_{j|1,\dots,j-1}}^{-2}, \quad (40)$$

and the covariance between the unconditional and conditional float ambiguities

$$\sigma_{\hat{N}_{k}\hat{N}_{j|1,...,j-1}} = \sigma_{\hat{N}_{k}\hat{N}_{j}} - \sum_{i=1}^{j-1} \sigma_{\hat{N}_{j}\hat{N}_{i|1,...,i-1}} \\ \cdot \sigma_{\hat{N}_{i|1,...,i-1}}^{-2} \sigma_{\hat{N}_{k}\hat{N}_{i|1,...,i-1}}.$$
(41)

Clearly, both the conditional variances and the covariances depend on the order of fixings. It can be easily shown that the conditional ambiguity estimates are uncorrelated, i.e.

$$\sigma_{\hat{N}_{k|1,\dots,k-1},\hat{N}_{l|1,\dots,l-1}} = 0 \quad \forall \, k \neq l.$$
(42)

Thus, the success rate of sequential ambiguity fixing can be efficiently computed from the product of one-dimensional cumulative Gaussian distributions, i.e.

$$P_{\rm s} = \prod_{k=1}^{K} \int_{-0.5}^{+0.5} \frac{1}{\sqrt{2\pi\sigma_{\hat{N}_{k|1,...,k-1}}^{2}}} \\ \cdot \exp\left(-\frac{(\varepsilon_{\hat{N}_{k|1,...,k-1}} - b_{\hat{N}_{k|1,...,k-1}})^{2}}{2\sigma_{\hat{N}_{k|1,...,k-1}}^{2}}\right) d\varepsilon_{\hat{N}_{k|1,...,k-1}}.$$
(43)

Bootstrapping as well as any other integer ambiguity resolution technique can be fully described by so called pullin regions [13]. A pull-in region represents the set of all float ambiguities  $\hat{N}$  that are mapped to the same integer vector  $\check{N}_k$ . The map  $S_{\check{N}_k}$  is given by

$$S_{\check{\boldsymbol{N}}_k} = \{ \hat{\boldsymbol{N}} \in \mathbb{R}^{K \times 1} | \check{\boldsymbol{N}}_k = S(\hat{\boldsymbol{N}}) \}, \quad \check{\boldsymbol{N}}_k = \mathbb{Z}^{K \times 1}.$$
(44)

These pull-in regions shall now be analyzed for the optimal integer least-squares estimator, which is defined as

$$\tilde{\boldsymbol{N}} = \arg\min_{\boldsymbol{N}} \|\hat{\boldsymbol{N}} - \boldsymbol{N}\|_{\boldsymbol{\Sigma}_{\tilde{N}}^{-1}}^2.$$
(45)

Fig. 3 shows these regions for a double difference carrier phase positioning over a large baseline with a good satellite geometry. Subfigure (a) refers to the estimation of the E1 integers and subfigure (b) to the widelane ambiguities.

Obviously, the increase in the wavelength from 19.0 cm to 3.285 m substantially increases the size of the pull-in regions. Both figures also the include the error ellipse given by  $\|\hat{N} - N\|_{\Sigma_{\hat{N}}}^2 = c$  with c = 3. Its size is larger than the size of the pull-in region for uncombined ambiguities but significantly smaller than the size of the widelane pull-in regions. This is another indication for extremely reliable ambiguity resolution with our linear combinations. The



(a) E1 pull-in regions with  $\lambda = 19.0$  cm



(b) Widelane pull-in regions with  $\lambda=3.285~{\rm m}$ 

**Fig. 3** Increase of pull-in regions with multi-frequency linear combinations

integer least-squares estimation can be efficiently performed with the Least-squares Ambiguity Decorrelation Adjustment (LAMBDA) method of Teunissen [12]. The size of the error ellipse in Fig. 3 is typical for a long-baseline kinematic positioning with a good satellite geometry and measurements from only a few epochs.

Fig. 4 shows the benefit of geometry-preserving ( $h_1 = 1$ ), ionosphere-free ( $h_2 = 0$ ) linear combinations for Wide-Area Real-Time Kinematics (WA-RTK). If no linear combinations are used, the baseline (once per epoch), the integer ambiguities (using bootstrapping with integer decorrelation), the tropospheric wet zenith delay and its rate, the ionospheric slant delays for all satellites and their rates have to be estimated from double difference measurements on at least two frequencies. Here, the wideband Galileo signals on E1 (CBOC modulation) and E5 (AltBOC modulated) were considered at a carrier to noise power of 45 dB-Hz. The small wavelength and the large number of unknown parameters result in a rather poor probability of wrong fixing, which varies between  $10^{-4}$  and 1 depending on the satellite geometry. This is far too much for Safetyof-Life critical applications where a failure rate of at most  $10^{-9}$  is required. Therefore, the use of an optimized multifrequency code carrier combination of maximum discrimination and of a code-only combination of minimum noise amplification is analyzed. As both linear combinations are ionosphere-free, the latter two parameter sets do not have to be estimated. Fig. 4 shows that the probability of wrong fixing can be reduced by several orders of magnitude due to the large wavelength of 3.285 m. The  $10^{-9}$  requirement is fulfilled for any satellite geometry.



**Fig. 4** Benefit of E1-E5 mixed code carrier linear combination for reliable integer ambiguity resolution

Fig. 5 shows the benefit of a different class of linear combinations: the geometry-free  $(h_1 = 0)$  ones, which eliminate also the clock offsets, orbital errors and tropospheric delay. The benefit is analyzed for differential positioning with triple frequency (E1, E5a, E5b) receiver-receiver single difference measurements of 20 s. If no linear combinations are used, the carrier phase integer ambiguities, the baseline (once/ epoch), the differential receiver clock offset (once/ epoch), the ionospheric slant delays and their rates, as well as the tropospheric wet zenith delay and its rate have to be estimated. In this traditional approach, the ambiguities were resolved sequentially according to (39) with integer decorrelation based on uncombined measurements. The use of the linear combinations significantly simplifies the ambiguity resolution: It directly provides an integer estimate that only has to be averaged over T epochs, i.e.

$$\hat{N}^{k} = \frac{1}{T} \sum_{t=1}^{T} \left( \frac{1}{\lambda} \sum_{m=1}^{M} \left( \alpha_{m} \lambda_{m} \phi_{m}^{k}(t) + \beta_{m} \rho_{m}^{k}(t) \right) \right)$$
$$\sim \mathcal{N} \left( N^{k} + b_{u}^{k}, \sigma_{\hat{N}^{k}}^{2} \right), \qquad (46)$$

with

$$\sigma_{\hat{N}^k} = \frac{\sigma}{\lambda\sqrt{T}} = \frac{1}{2D\sqrt{T}},\tag{47}$$

and thus justifies also the maximization of the ambiguity discrimination D. As geometry-free linear combinations imply an independant fixing of the ambiguities from all satellites, the probability of wrong fixing can be efficiently computed from

$$P_{\rm s} = \prod_{k=1}^{K} \int_{-0.5}^{+0.5} \frac{1}{\sqrt{2\pi\sigma_{\hat{N}_k}^2}} \cdot e^{-\frac{(\varepsilon_{\hat{N}_k} - b_{\hat{N}_k})^2}{2\sigma_{\hat{N}_k}^2}} d\varepsilon_{\hat{N}_k}.$$
 (48)

Fig. 5 shows that this probability of wrong fixing is almost constant over time and enables a substantial improvement over the traditional approach especially for poor satellite geometries.



Fig. 5 Benefit of geometry-free, ionosphere-free linear combinations for integer ambiguity resolution

### SUCCESS RATE DETERMINATION FOR ROUN-DING OF FLOAT SOLUTION

Simple rounding of the float solution has recently received little attention mainly for two reasons: First, it provides a lower success rate than sequential bootstrapping and integer least-squares estimation for unbiased measurements. Secondly, there does not exist a closed-form expression for the evaluation of the success rate of rounding. Therefore, the easily computable success rate of bootstrapping became the de-facto standard, either used as a lower bound for integer least-squares estimation or directly used to characterize bootstrapping.

However, the simple rounding could be an interesting candidate for precise point positioning as it is less sensitive with respect to unknown biases than sequential ambiguity fixing and integer least-squares estimation. The sequential estimation accumulates the biases of various satellites, the integer decorrelation further amplifies them, and the search might additionally reduce the success rate due to the negligence of biases. The simple rounding prevents all these disadvantages. Consequently, there is a need for an efficient computation of the success rate of rounding as Monte-Carlo simulations are practically unacceptable for error rates in the order of magnitude of  $10^{-9}$ . Genz suggested in [10] an efficient method for the evaluation of the multivariate cumulative normal distribution. This method uses three integral transformations and shall be applied for the evaluation of the success rate which is given by

$$P_{\rm s} = P([\hat{N}] = N) = \frac{1}{\sqrt{|\Sigma_{\hat{N}}|(2\pi)^{K}}}$$
$$\cdot \int_{-0.5-b_{1}}^{+0.5-b_{1}} \dots \int_{-0.5-b_{K}}^{+0.5-b_{K}} e^{-\frac{1}{2}\varepsilon_{\hat{N}}^{T}\Sigma_{\hat{N}}^{-1}\varepsilon_{\hat{N}}} d\varepsilon_{\hat{N}_{1}} \dots d\varepsilon_{\hat{N}_{K}},$$
(49)

where  $\varepsilon_{\hat{N}} = \hat{N} - N$  denotes the error of the float solution  $\hat{N}$ . It is normal distributed, i.e.

$$\varepsilon_{\hat{N}} \sim \mathcal{N}\left(\mathbf{0}, \boldsymbol{\Sigma}_{\hat{N}}\right),$$
 (50)

with the float ambiguity covariance matrix  $\Sigma_{\hat{N}}$ . The Choleskey decomposition is used to diagonalize the error vector, i.e.

$$\boldsymbol{e}_{\hat{\boldsymbol{N}}} = \boldsymbol{C}^{-1} \boldsymbol{\varepsilon}_{\hat{\boldsymbol{N}}},\tag{51}$$

with

$$\boldsymbol{\Sigma}_{\hat{N}} = \boldsymbol{C}\boldsymbol{C}^T. \tag{52}$$

Thus, the success rate of (49) can be rewritten as

$$P_{\rm s} = \frac{1}{\sqrt{(2\pi)^K}} \int_{l_1}^{u_1} e^{-\frac{e_{\hat{N}_1}^2}{2}} \int_{l_2(e_{\hat{N}_1})}^{u_2(e_{\hat{N}_1})} e^{-\frac{e_{\hat{N}_2}^2}{2}} \dots$$
$$\cdot \int_{l_K(e_{\hat{N}_1},\dots,e_{\hat{N}_{K-1}})}^{u_K(e_{\hat{N}_1},\dots,e_{\hat{N}_{K-1}})} e^{-\frac{e_{\hat{N}_K}^2}{2}} de_{\hat{N}_1} de_{\hat{N}_2} \dots de_{\hat{N}_{K-1}},$$
(53)

where the correlation between the float ambiguities is included in the integration limits  $l_k$  and  $u_k$ . These limits are obtained from the inequalities

$$-0.5 - b_k \le \varepsilon_{\hat{N}_k} = \sum_{j=1}^k C_{kj} e_{\hat{N}_j} \le +0.5 - b_k, \quad (54)$$

which can be solved for  $e_{\hat{N}_{h}}$ :

$$l_k \le e_{\hat{N}_k} \le u_k \tag{55}$$

with

$$l_{k} = \frac{-0.5 - b_{k} - \sum_{j=1}^{k-1} C_{kj} e_{\hat{N}_{j}}}{C_{kk}}$$
$$u_{k} = \frac{+0.5 - b_{k} - \sum_{j=1}^{k-1} C_{kj} e_{\hat{N}_{j}}}{C_{kk}}.$$
 (56)

The second transformation uses the cumulative normal distribution to absorb the exponential functions of (53), i.e.

$$z_k = \Phi(e_{\hat{N}_k}),\tag{57}$$

with

$$\Phi(\nu) = \frac{1}{\sqrt{2\pi}} \int_{-\infty}^{\nu} e^{-\frac{1}{2}\theta^2} d\theta.$$
 (58)

Thus, (53) simplifies to

$$P_{\rm s} = \int_{l_1'}^{u_1'} \int_{l_2'(z_1)}^{u_2'(z_1)} \dots \int_{l_K'(z_1,\dots,z_{K-1})}^{u_K'(z_1,\dots,z_{K-1})} dz_1 dz_2 \dots dz_K,$$
(59)

with the transformed integration limits

$$l'_{k} = \Phi\left(\frac{1}{C_{kk}}\left(-0.5 - b_{k} - \sum_{j=1}^{k-1} C_{kj}\Phi^{-1}(z_{j})\right)\right)$$
$$u'_{k} = \Phi\left(\frac{1}{C_{kk}}\left(+0.5 - b_{k} - \sum_{j=1}^{k-1} C_{kj}\Phi^{-1}(z_{j})\right)\right).$$

Finally, Genz's third transformation is given by

$$w_k = \frac{z_k - l'_k}{u'_k - l'_k},\tag{60}$$

which puts the integral into a constant limit form, i.e.

$$P_{\rm s} = (u_1' - l_1') \int_0^1 (u_2' - l_2') \int_0^1 \dots (u_K' - l_K') \int_0^1 dw_1 dw_2 \dots dw_K.$$
(61)

Eq. (61) can be expanded to

$$P_{\rm s} = (u_1' - l_1') \int_0^1 (u_2' - l_2') f(w_1) \int_0^1 \dots (u_K' - l_K') f(w_{K-1}) \int_0^1 f(w_K) dw_1 \dots dw_K,$$
(62)

with

$$f(w_k) = \begin{cases} 1 & \text{if } 0 \le w_k \le 1\\ 0 & \text{else.} \end{cases}$$
(63)

The introduction of  $f(w_k)$  does not change the value of  $P_s$  but it allows us to interpret  $w_k$  as a uniformly distributed random variable between 0 and 1. Thus, (62) can also be written as

$$P_{s} = E_{w_{1},...,w_{K}} \left\{ \prod_{k=1}^{K} (u_{k}'(w_{1},...,w_{K}) - l_{k}'(w_{1},...,w_{K})) \right\}$$
(64)

with  $w_k \sim \mathcal{U}(0, 1)$  for all k. The success rate of (64) can be efficiently computed using Monte-Carlo simulation or more advanced numerical integration techniques, e.g. the subregion adaptive method as discussed by Genz in [10]. Fig. 6 shows the benefit of computing the expectation value w.r.t.  $w_k$  in (64) instead of w.r.t.  $\varepsilon_{\hat{N}}$  in (49). The computational burden is measured by the time required to estimate  $P_{\rm s}$  with a dual core 2.1 GHz CPU. The use of the three integral transformations enables a substantial reduction in the computation time. A realtime evaluation becomes also feasible.



**Fig. 6** Efficient computation of success rate of rounding with integral transformations.

Fig. 7 shows the probability of wrong fixing for various integer estimation techniques. An ionosphere-free carrier smoothing is applied to two GP-IF linear combinations (a code carrier combination of maximum discrimination and a code-only combination) of E1 and E5 measurements to improve the reliability of widelane ambiguity resolution. Obviously, a larger smoothing period results in a lower error rate. For unbiased measurements, the integer least-squares estimation achieves the lowest error rate of all fixing methods. A slightly higher error rate can be observed for sequential fixing with integer decorrelation due to the lack of an integer search. An additional degradation occurs if the integer decorrelation is omitted, and the largest error rate is obtained for rounding as it does not consider the correlations between the float ambiguity estimates. The ranking of the fixing techniques completely changes in the presence of biases. An elevation dependent exponential bias profile was chosen to analyze the impact of multipath. A worstcase accumulation over all visible satellites is considered as described by Henkel et al. in [7]. The magnitude of the code multipath was set to 1 cm for a satellite in the zenith and to 10 cm for a satellite in the horizon. For the phase multipath, 0.01 cycles and 0.1 cylces were assumed respectively. In this case, rounding achieves the lowest error rate, followed by sequential fixing without and with integer decorrelation. The integer decorrelation amplifies the biases and the search criterion is suboptimal which results in the largest error rate. Consequently, the most simple method is also the most robust one: the rounding of the float solution.



**Fig. 7** Comparison of various integer ambiguity resolution techniques for both unbiased and biased measurements with worst-case accumulation of biases.

### CONCLUSION

In this paper, a new group of linear combinations was analyzed that include both code and carrier phase measurements on two or more frequencies. An arbitrary scaling of the geometry, an arbitrary scaling of the ionospheric delay, and any preferred wavelength can be obtained with these linear combinations. The maximization of the ambiguity discrimination leads to combinations with a wavelength of several meters and a noise level of a few centimeters. The integer ambiguities of these combinations can be resolved with a probability of wrong fixing of less than  $10^{-9}$  with measurements from a few epochs. These combinations are recommended for any application where reliability is more important than accuracy.

Moreover, an efficient method for the computation of the success rate of rounding of the float solution is suggested. It is based on a transformation of the cumulative multivariate Gaussian distribution into uniform distributions, which can be efficiently evaluated in realtime. The rounding of the float solution was considered for two reasons: First, the linear combinations improve the conditioning of the equation system such that there is no strong need of an integer decorrelation. Secondly, rounding of the float solution is much less sensitive with respect to multipath and biases than bootstrapping and integer least-squares estimation.

Both the optimized multi-frequency linear combinations with large wavelengths and the efficient computation of the success rate are seen as two steps to improve the reliability of ambiguity resolution for precise point positioning.

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